

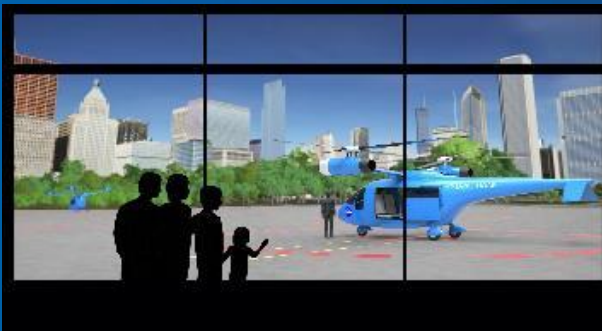


A Brief History of Rotorcraft Aeroacoustics

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Categories of Rotorcraft Noise

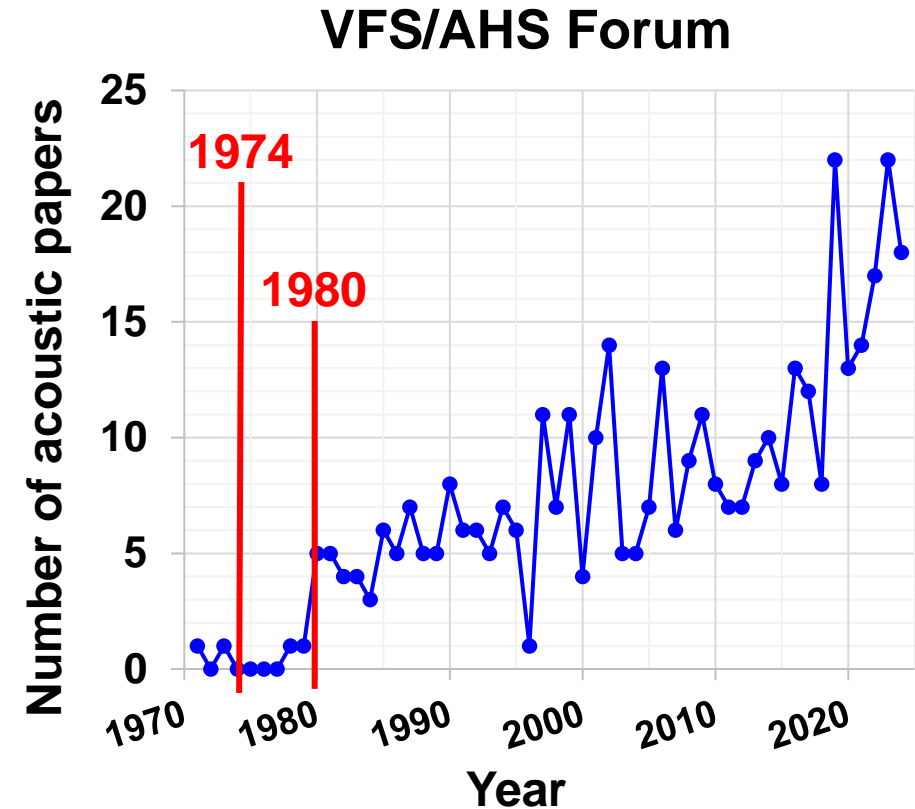


- **Thickness**
- **Loading**
 - Steady
 - Unsteady
 - Blade Vortex Interaction (BVI)
 - Broadband
- **High Speed Impulsive**

- Introduction
 - VFS/AHS Forums
- History
 - Early acoustics (1747 – 1878)
 - Advent of aeroacoustics (1822 – 1952)
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 - Summary of noise sources
- Computational contributions
- Experimental contributions
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 - Wind tunnel testing
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- **VFS/AHS Forum**

- **1980:** First Acoustic Session for Forum 26 in Washington DC with (5 papers)
- **2016:** 29th Alexander A. Nikolsky Honorary Lecture by Schmitz
- **2020:** Best Forum paper “Development and Validation of Generic Maneuvering Flight Noise Abatement Guidance for Helicopters”, by Stephenson, Watts, Greenwood, and Pascioni



- **Technical Fellows:** Schmitz (1993), Leverton (1995), Brooks (2000), Tung (2006), Farassat (2011), JanakiRam (2014), Boyd (2021), and Brentner (2022)
- **Various other AHS/VFS specialist conferences included acoustic sessions**

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- **1747:** Classical wave equation derived by Jean-Baptiste le Rond d'Alembert

$$\frac{\partial^2 u}{\partial t^2} = c^2 \frac{\partial^2 u}{\partial x^2}$$

- **1878:** Strouhal found that the frequency (f) was related to the velocity (u), a characteristic length of the string (d), and the diameter of the string

$$f = 0.185 \frac{u}{d}$$



- **1822:** Aerodynamics begins with Navier-Stokes equations by expressing momentum equilibrium with conservation of mass
- **1952:** Sir James Lighthill's theory rearranged mass and momentum equation to create a wave equation with sources
 - Did not include surfaces, only considers turbulence

$$\mathbf{T}_{ij} = \rho \mathbf{v}_i \mathbf{v}_j + \sigma_{ij} - c^2 \rho' \delta_{ij}$$

Lighthill's theory was a catalyst to revolutionize the aeroacoustics field for jet engine aeroacoustics



- **1936:** Gutin analyzed sound produced by a 2-bladed airplane propeller (dipole)
- **1937:** Deming derived thickness noise formulation (monopole)
- **1954:** Garrick and Watkins extended Gutin's work to account for forward motion for a propeller
- **1969:** Lawson and Ollerhead took Gutin's work and applied it to helicopter main rotor noise

Other notable contributors include Yudin, Lyon, Lilley, Sharland, Hulse, and others

Beginnings of Modern Rotorcraft Aeroacoustics



- **1969:** Ffowcs-Williams and Hawkins (FWH), rearranged the Navier-Stokes equations to an inhomogeneous wave equation for the density, with two surface terms and a volume source term



<https://www.youtube.com/watch?v=8BmESsMroRM>

$$\left(\frac{1}{c_s^2} \frac{\partial^2}{\partial t^2} - \nabla^2 \right) \tilde{p} = \frac{\partial^2}{\partial x_i \partial x_j} \left(T_{ij} H(\mathbf{f}) \right) - \frac{\partial}{\partial x_i} \left(\ell_i |\nabla \mathbf{f}| \delta(\mathbf{f}) \right) + \frac{\partial}{\partial t} \left(\rho_0 v_n |\nabla \mathbf{f}| \delta(\mathbf{f}) \right)$$

In the 1960's, the increasing use of helicopters for U.S. military applications and later commercial certification requirements which resulted in a demand in an expansion for rotorcraft acoustics research

- **1980:** Farassat re-derived FWH using generalized functions and then derived solutions to the FWH equation using various acoustic analogies along with methods to solve the wave equation using Green's Functions
 - Numerous Formulations of Farassat exists (F1, G1, G1A, F2B, etc.), but F1A is the one *most used* in rotorcraft applications
 - F1A uses impermeable subsonic surfaces and neglects quadrupole term

Thickness noise term

$$4 \pi p'_{\text{T}}(\mathbf{x}, t) = \int_{f=0} \left[\frac{\rho_0 \dot{v}_n}{r (1 - M_r)^2} + \frac{\rho_0 v_n \hat{r}_i \dot{M}_i}{r (1 - M_r)^3} \right]_{\text{ret}} dS + \int_{f=0} \left[\frac{\rho_0 c v_n (M_r - M^2)}{r^2 (1 - M_r)^3} \right]_{\text{ret}} dS$$

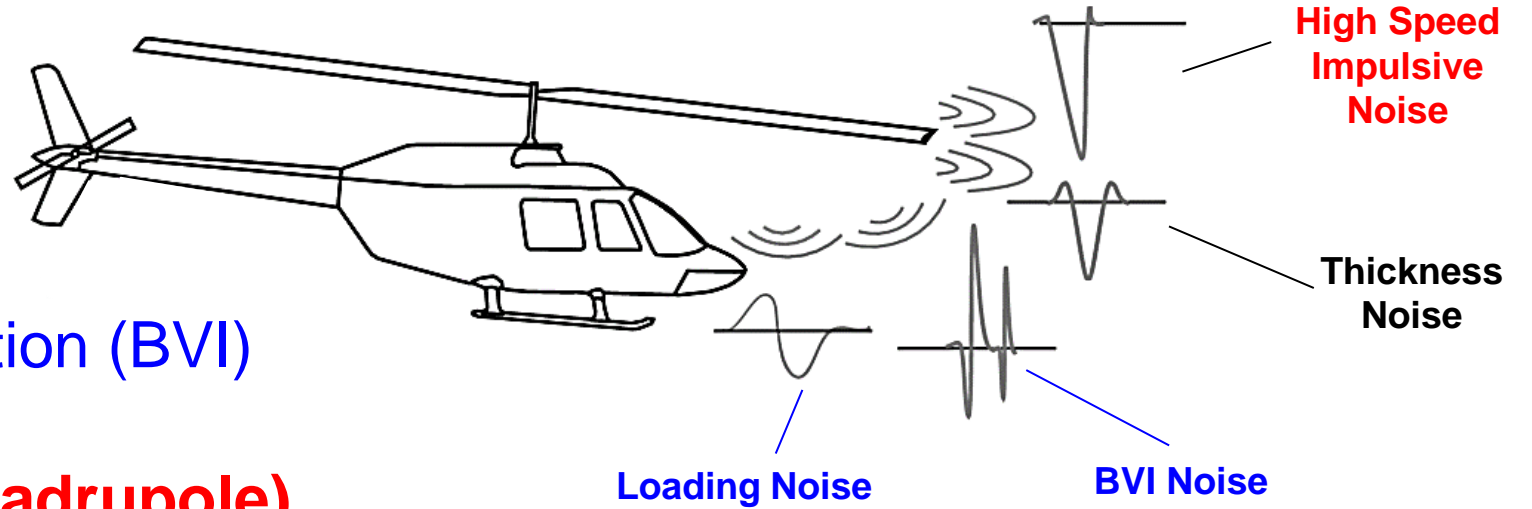
Loading noise term

$$4 \pi p'_{\text{L}}(\mathbf{x}, t) = \int_{f=0} \left[\frac{\dot{p} \cos \theta}{c r (1 - M_r)^2} + \frac{\hat{r}_i \dot{M}_i p \cos \theta}{c r (1 - M_r)^3} \right]_{\text{ret}} dS + \int_{f=0} \left[\frac{p (\cos \theta - M_i n_i)}{r^2 (1 - M_r)^2} + \frac{(M_r - M^2) p \cos \theta}{r^2 (1 - M_r)^3} \right]_{\text{ret}} dS$$

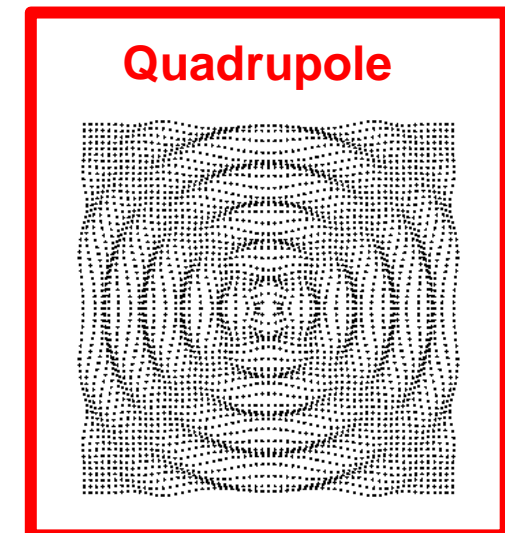
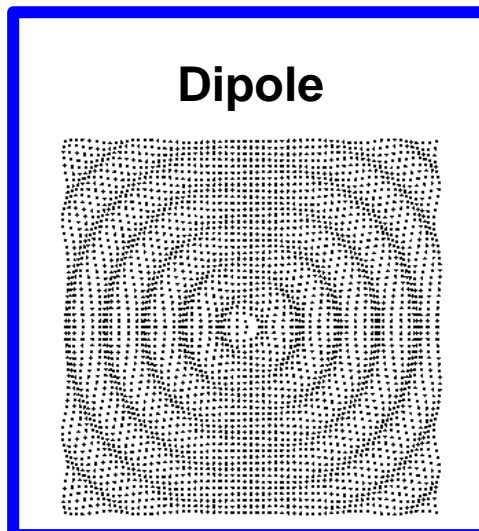
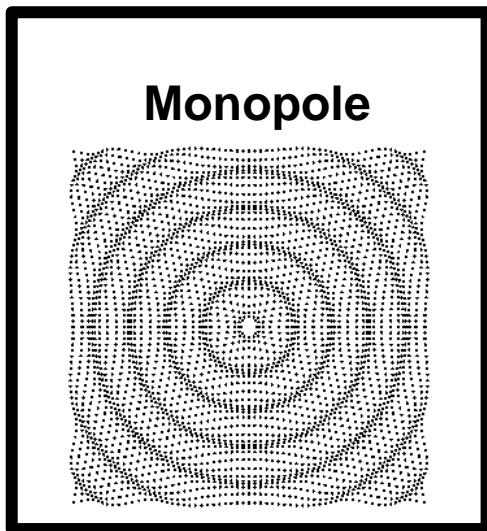
Summary of Rotor Noise Sources



- **Thickness (monopole)**
- **Loading (dipole)**
 - Steady
 - Unsteady
 - Blade Vortex Interaction (BVI)
 - Broadband
- **High Speed Impulsive (quadrupole)**

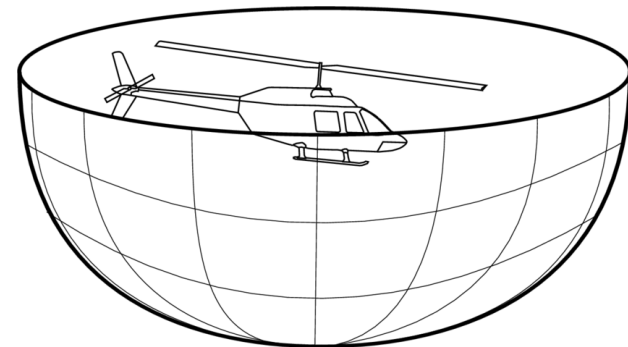


Greenwood (2011)



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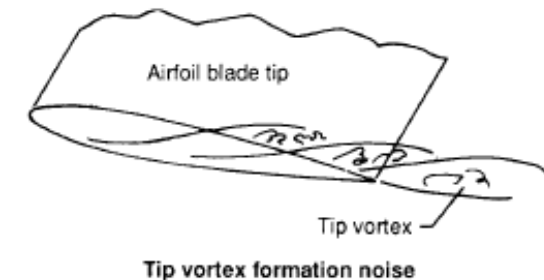
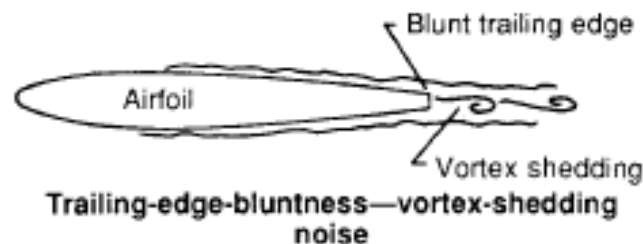
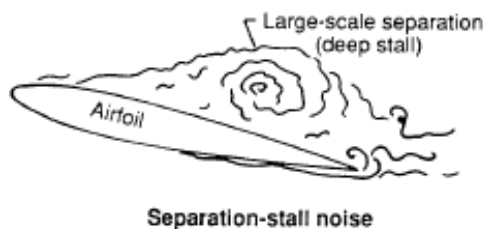
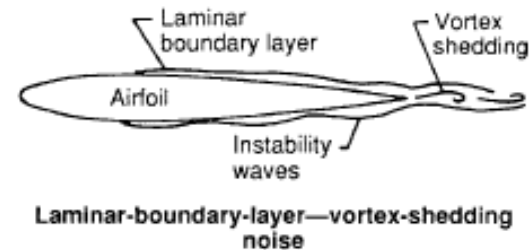
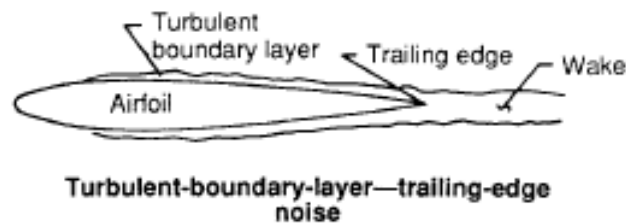
- **1986:** NASA development the *first widely* used rotor noise prediction code WOPWOP using F1A
- **1986 - present:** Various rotor acoustic prediction tools have been developed providing their own pros and cons beyond WOPWOP, such as PSU-WOPWOP, ANOPP2, UCD-Quietly, etc.
- Efforts of providing input from available/limited data have evolved including compact thickness, compact loading, full surface data from CFD, etc.
- How acoustic results are presented has evolved (e.g., hemispheres and spectrograms)



Computational Contributions: Empirical Models



- **1933:** Stowell and Deming looked at rods spinning (spinning like rotor blades) and found that the acoustic power (P) was related to the tip speed (V_{Tip}) to the power of 5.5
- **1989:** Brooks, Pope, and Marcolini (BPM) developed semi-empirical prediction method for self noise. BPM used within acoustic prediction tools





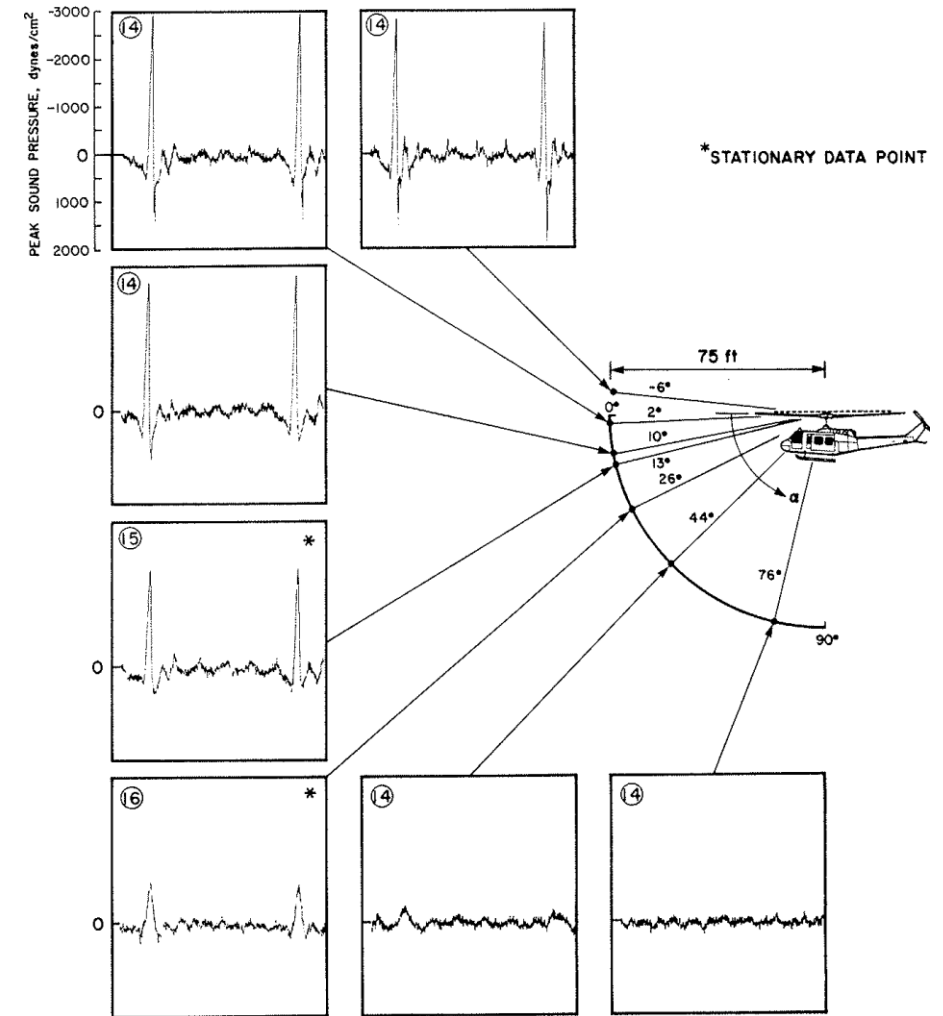
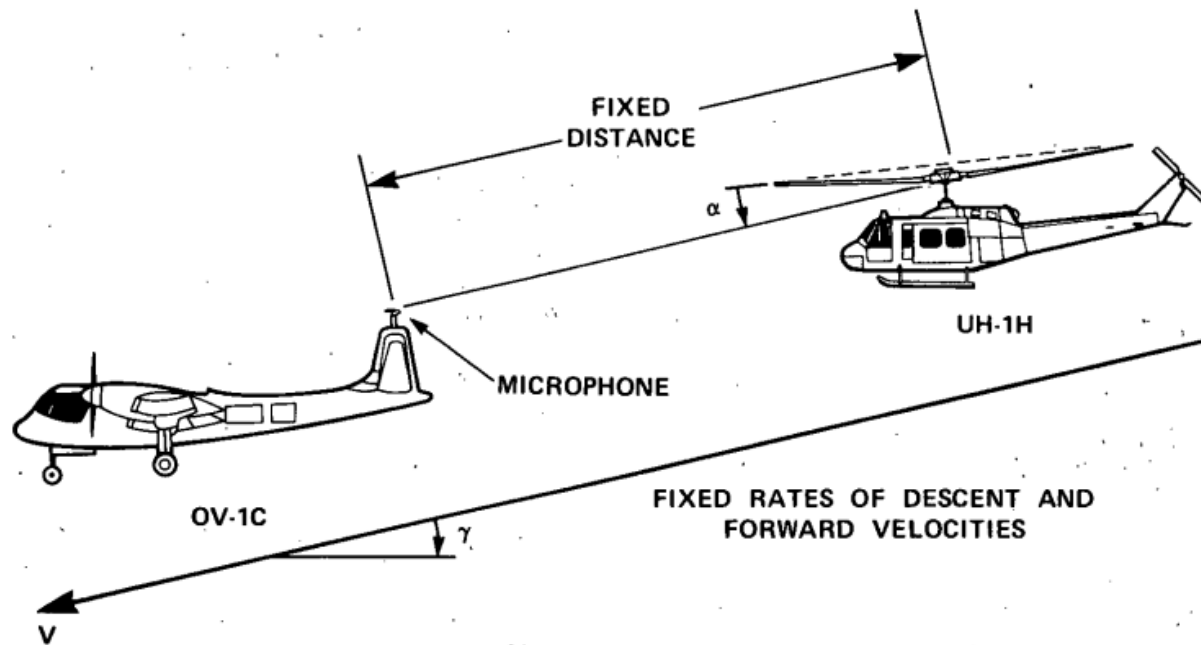
Advancements to comprehensive analysis, CFD/CSD Coupling, and CFD, are critical due to F1A input requirements (surface motion and surface loading), many efforts have been made to advance and validate such efforts

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Experimental Contributions: Flight Testing



- **1976:** Schmitz and Boxwell acquires far-field UH-1H acoustic measurements by placing a microphone on the tail of an OV-10C quiet aircraft
 - Showed differences in pulse behavior for various rotor noise sources



Experimental Contributions: Flight Testing



- **1991 - 1995:** In-Flight Rotorcraft Acoustics Program (IRAP) used microphones on the wing tips (matching wind-tunnel measurement locations) and tail fin of the YO-3A and acquired measurements from the following aircraft:
 - S-76C (1991 - 1992)
 - BO 105 (1993)
 - UH-60A (1993 - 1994)
 - XV-15 (1995)



S-76C



BO 105



UH-60A

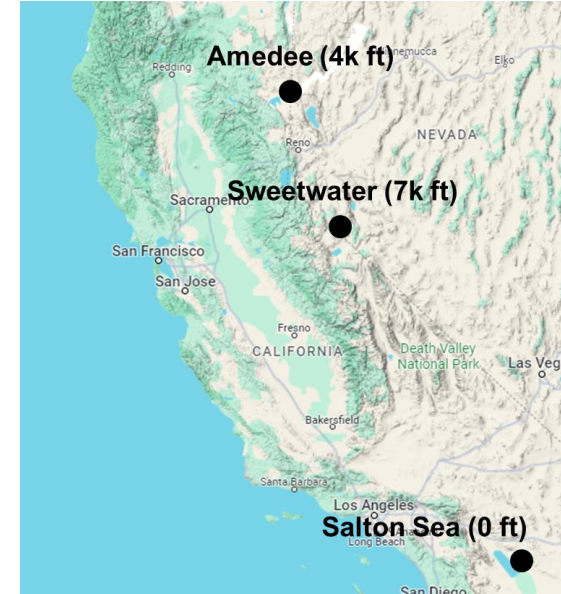


XV-15

Experimental Contributions: Flight Testing



- **2015:** NASA and the U.S. Army performed a flight test for the AS350 SD1 and EH-60L to investigate the effects of altitude variation
 - 3 test sites (0, 4k, and 7k feet above mean SL)
- **2016 - 2019:** NASA, FAA, and the U.S. Army conducted the Maneuver Acoustics Test for 6 helicopters and then later for 4 helicopters
 - Characterized source for maneuver and approach

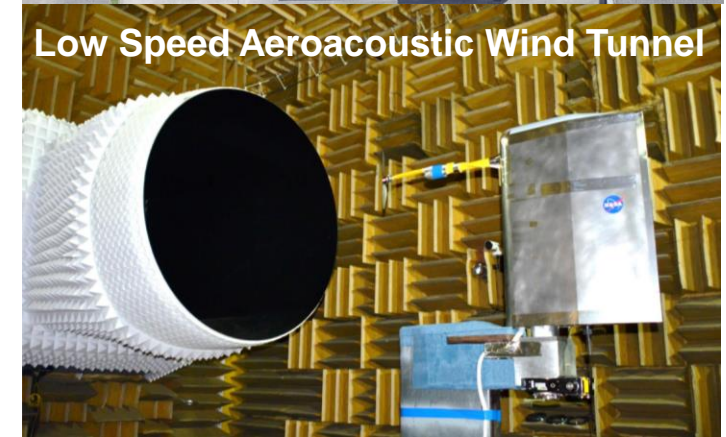
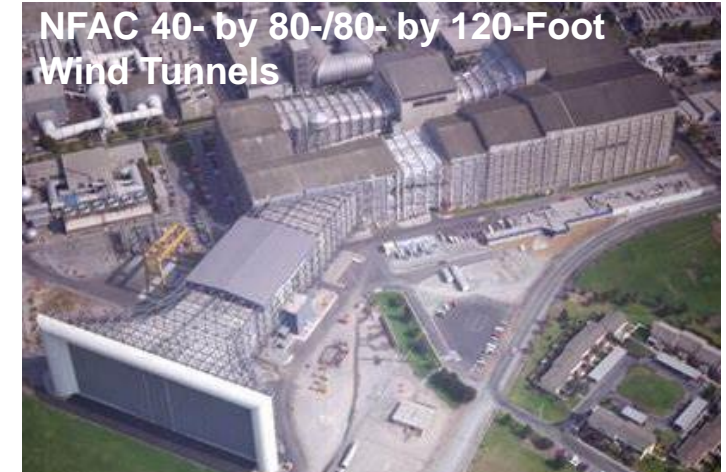


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Wind Tunnels Used for Rotor Testing



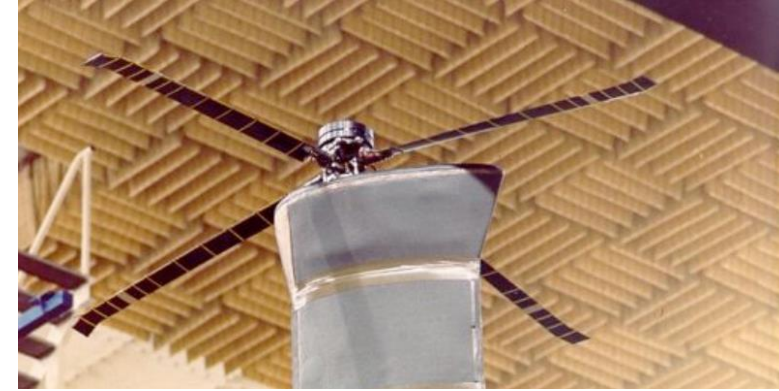
- **Examples of anechoic wind tunnels used for rotor acoustic testing include:**
 - National Full-Scale Aerodynamics Complex (NFAC) 40- by 80-/80- by 120-Foot Wind Tunnels (Ames)
 - German-Dutch Wind Tunnel (DNW)
 - Low Speed Aeroacoustic Wind Tunnel (LSWAT) (Langley)



Experimental Contributions: Wind Tunnel Testing



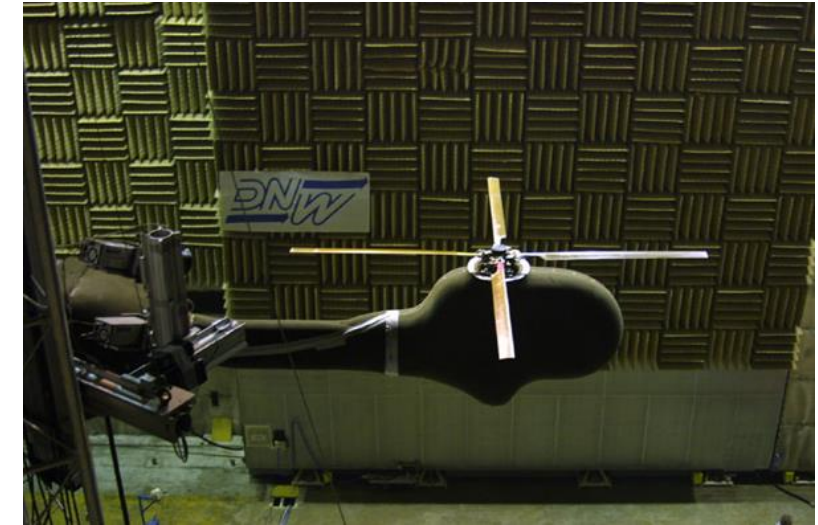
- **1989 - 2009:** NASA/Army UH-60A Airloads Program
 - **1989:** Model-scale rotor tested in DNW wind tunnel
 - **1993 - 1994:** Flight test
 - **2009:** Full-scale rotor tested in NFAC 40- by 80-Foot Wind Tunnel (same rotor used from flight vehicle)
 - Led to long running workshop (for analysis of experimental data, prediction/computation improvements, etc.)



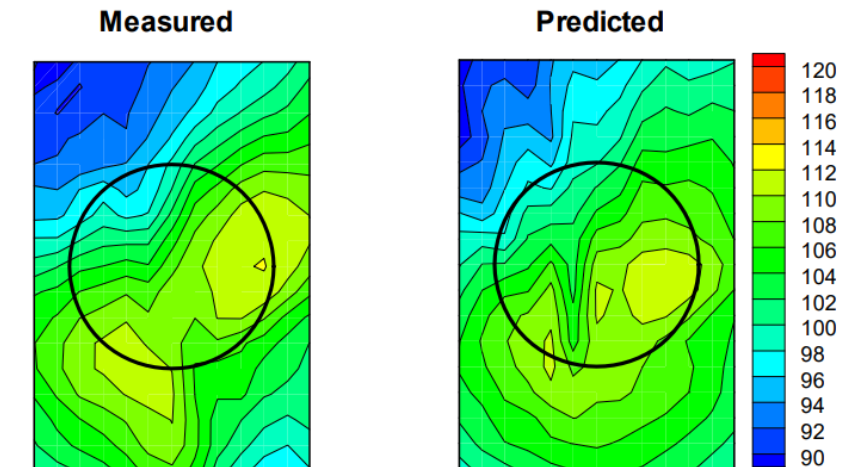
Experimental Contributions: Wind Tunnel Testing



- **1994/2001:** Higher Harmonic Control Acoustic Rotor Test (HART I and HART II) test in DNW International program
 - Objective to understand rotor BVI noise generation/reduction mechanisms with higher-harmonic blade-pitch control inputs of a scaled BO 105 rotor
 - Extensive acoustic and wake flow field measurements
 - Led to a decade of workshops



HART-II: 3P HHC, phase = 120°
Mid-Frequency Noise

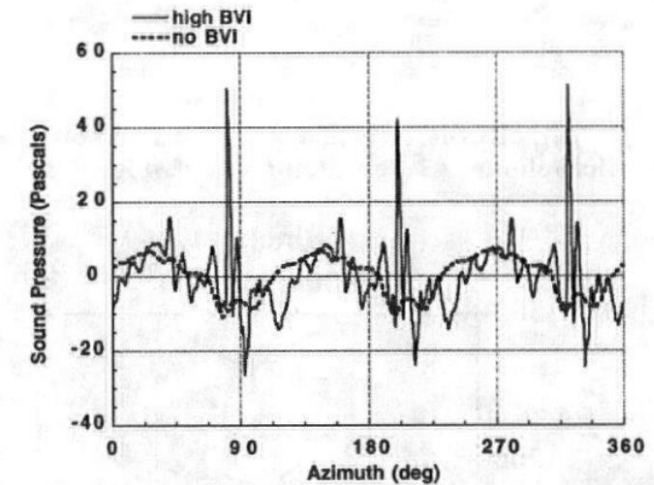


Experimental Contributions: Wind Tunnel Testing



- **1997:** XV-15 rotor in the NFAC 80- by 120-Foot Wind Tunnel
 - Acquired baseline BVI noise and performance measurements for typical descending flight conditions

- **1998:** Tilt Rotor Aeroacoustic Model (TRAM) test in the DNW for a single ¼-scale tiltrotor in hover, helicopter flight, and low speed axial flight
 - Performance, airloads, structural loads, acoustics



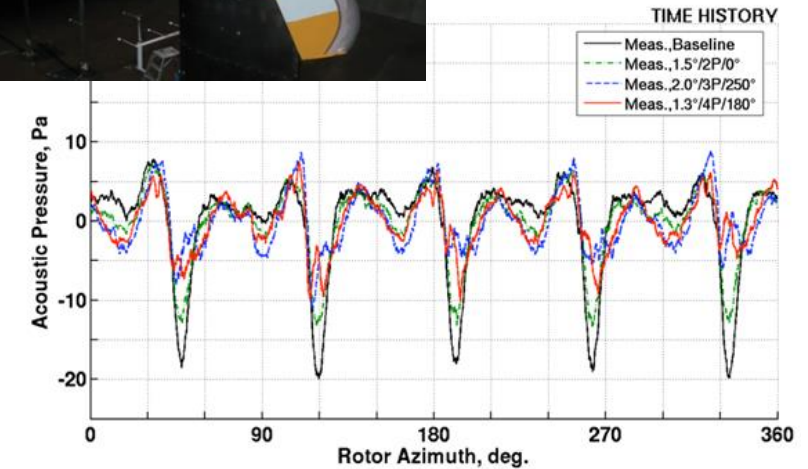
Experimental Contributions: Wind Tunnel Testing



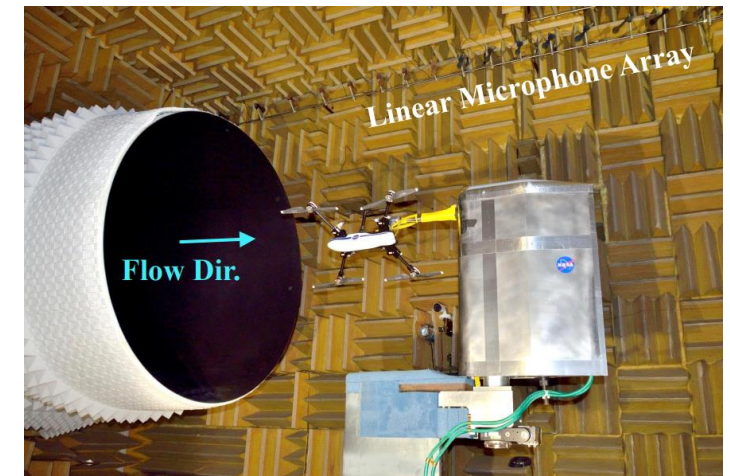
- **2009:** Boeing SMART rotor in the NFAC 40-by 80-Foot Wind Tunnel Full-Scale MD 900 Explorer rotor
 - On-blade piezoelectric actuators driving trailing edge flaps
 - Thickness noise peak levels are reduced by up to 50% (via directivity)



	OASPL, dB
Meas., Baseline :	109.87
Meas., 1.5°/2P/0° :	107.10
Meas., 2.0°/3P/250° :	105.01
Meas., 1.3°/4P/180° :	104.50



- **2015 - 2018:** Testing of small Unmanned Aerial Vehicles (UAVs) (< 55 lbs.) in the LSAWT



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Urban Air Mobility: Testing



- **2022:** Moog Surefly hover flight test at Cincinnati Municipal Airport
- **2022:** Joby Aviation preproduction all-electric vertical takeoff and landing prototype flight test
- **2023:** Single Joby full-scale propeller tested in the NFAC 40- by 80-Foot Wind Tunnel



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- **Experimental**

- Need for more comprehensive data (high quality blade motion, blade loading, wake measurements, etc.)
- Multi-rotor test articles
- Improvements to measurement hardware (microphones, microphone stands, DAQ, tunnel improvements, etc.)

- **Computation**

- Robust and reliable prediction of rotorcraft acoustics
- Take advantage of future high computer capabilities

Acknowledgements



- VFS acoustics committee
- NASA Ames Aeromechanics Office and interns

